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# Effect of borate glass additives on the sintering behaviour and dielectric properties of BaTi<sub>4</sub>O<sub>9</sub> ceramics

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### Abstract

Effect of  $B_2O_3$  and  $BaB_2O_4$  addition on microwave dielectric characteristics and sintering behaviours of  $BaTi_4O_9$  ceramics were investigated. When  $B_2O_3$  was added, bulk density of the sintered sample decreased as the content of  $B_2O_3$  increased.  $B_2O_3$  addition induced complex reaction with  $BaTi_4O_9$  and resulted in the development of second phases such as  $Ba_2Ti_9O_{20}$ ,  $BaTi(BO_3)_2$  and  $TiO_2$ . When  $BaB_2O_4$  was added, however, relative density increased and the second phases of  $Ba_2Ti_9O_{20}$  and  $BaTi(BO_3)_2$  were produced. Dielectric characteristics of  $BaTi_4O_9$  were also discussed from the viewpoint of bulk density, microstructure and second phases. © 2005 Elsevier Ltd. All rights reserved.

Keywords: Sintering; Microstructure-final; Dielectric properties; Borides; BaTi<sub>4</sub>O<sub>9</sub>

#### 1. Introduction

Because of proper microwave dielectric properties of BaO–TiO<sub>2</sub> based systems, a number of researches have been carried out for the development and application for commercial units. In the case of BaTi<sub>4</sub>O<sub>9</sub>, which has superior dielectric properties for high frequency applications, very high sintering temperature around 1300 °C was required for the proper densification. For the application to low temperature co-firing technology, low-melting glasses were often used for lowering the sintering temperatures.

Various kinds of low-melting glasses have been used in  $BaTi_4O_9$  ceramics.<sup>1,2</sup> Even though the resultant performance of dielectrics with glass additions greatly depends on the chemical reaction between the glasses and dielectrics, densification and microstructure, no systematic studies have been conducted. In this study,  $B_2O_3 - a$  well-known liquid former – was employed for a lower temperature sintering of  $BaTi_4O_9$ . During sintering considerable chemical reactions between  $B_2O_3$  and  $BaTi_4O_9$  were expected to occur when Ba and Ti components were dissolved out form the  $BaTi_4O_9$ . From this point of view, when another boron based low melting glass of  $BaB_2O_4$  is added, the chemical reaction thought to be different because the Ba component already exists in  $BaB_2O_4$ .

0955-2219/\$ - see front matter © 2005 Elsevier Ltd. All rights reserved. doi:10.1016/j.jeurceramsoc.2005.09.081 In the present study, two kinds of borides,  $B_2O_3$  and  $BaB_2O_4$ , were added for lowering the sintering temperature of  $BaTi_4O_9$ . The phase development behavior, densification, microstructure and dielectric characteristics were examined.

## 2. Experimental procedure

BaTi<sub>4</sub>O<sub>9</sub> was prepared by the conventional solid-state reaction process using high purity chemicals of  $BaCO_3$  (99.95%) and TiO<sub>2</sub> (99.9%). After ball milling and drying, the mixtures were calcined at 1100 °C for 2h. BaB<sub>2</sub>O<sub>4</sub> was prepared using BaCO<sub>3</sub> and B<sub>2</sub>O<sub>3</sub> (99.9%) through a heat treatment at 1150 °C for 1 h in a Pt crucible. Calcined BaTi<sub>4</sub>O<sub>9</sub> and additives of B<sub>2</sub>O<sub>3</sub> and BaB<sub>2</sub>O<sub>4</sub> were dry-mixed for 24 h. The granulated powders were then pressed into pellets under the pressure of 100 MPa. The specimens were sintered in the temperature range of 900-1100 °C for 2 h in air. Powder X-ray diffraction with nickel-filtered Cu Kα radiation (Mac Science, M03XHF, Japan) was conducted on the sintered specimens to identify the phases. Microstructure observation was conducted by using a scanning electron microscope (JEOL 4500, Japan). Microwave dielectric properties were measured by the parallel plate method originally proposed by Hakki and Coleman<sup>3</sup> utilizing TE<sub>01δ</sub> resonant mode using a network analyzer (Agilent 8719ES S-parameter, USA). The quality factor  $(Q \times f)$  and the temperature coefficient of resonant frequency  $(\tau_f)$  were measured by the open cavity resonator method<sup>4</sup> using HP8720C network analyzer.

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### 3. Results and discussion

Fig. 1 shows the X-ray diffraction patterns of the sintered samples with (a) 9 wt%  $B_2O_3$ ; and (b) 9 wt%  $BaB_2O_4$  as a function of sintering temperature. In the case of  $B_2O_3$  added samples, it was mostly composed of  $BaTi_4O_9$  phase with small amount of  $BaTi(BO_3)_2$  and  $TiO_2$  when it was sintered at 800 °C. However,  $BaTi_4O_9$  disappeared and  $Ba_2Ti_9O_{20}$  phase appeared as the main crystalline phase together with small amount of  $BaTi(BO_3)_2$  at the higher sintering temperatures. In the case of the samples with  $BaB_2O_4$  addition,  $BaTi_4O_9$  was the major phase at the sintering temperatures of 800 and 900 °C. When the sintering temperature was elevated to 950 °C or above,  $Ba_2Ti_9O_{20}$  became dominant and small amount of  $BaTi(BO_3)_2$  coexisted.

Fig. 2 shows the volume fraction of the phases in the samples sintered at  $1050 \,^{\circ}$ C for 2 h as a function of  $B_2O_3$  and  $BaB_2O_4$  content. These results were determined using the integrated intensity of major X-ray diffraction peaks of respective phases. When the content of  $B_2O_3$  is increased from 1 to 9 wt%, the volume fraction of  $Ba_2Ti_9O_{20}$  drastically decreased from 62.1 to 10.2%, but that of  $Ba_2Ti_9O_{20}$  slowly decreased from 89.6 to 64.8% when the content of  $B_2O_3$  around 450 °C, when  $BaTi_4O_9$  grains are surrounded by  $B_2O_3$  liquid, Ba and Ti ions will be



Fig. 1. XRD diffraction patterns of  $BaTi_4O_9$  samples as a function of sintering temperature for the cases with: (a) 9 wt%  $B_2O_3$ ; and (b) 9 wt%  $BaB_2O_4$  ( $\bigcirc$ ,  $BaTi(BO_3)_2$ ;  $\bullet$ ,  $TiO_2$ ;  $\blacksquare$ ,  $Ba_2Ti_9O_{20}$ ;  $\Box$ ,  $BaTi_4O_9$ ).



Fig. 2. Change in the volume fraction of the phases in the samples sintered at 1050 °C for 2 h as a function of: (a) B<sub>2</sub>O<sub>3</sub>; and (b) BaB<sub>2</sub>O<sub>4</sub> content.

concurrently dissolved out into  $B_2O_3$  melts from  $BaTi_4O_9$  grains and then forms Ba-Ti-B-O glass during the sintering process at elevated temperatures. In the Ba-Ti-B-O glass, B and Ba component act as glass network former and modifier, respectively. However, because the solubility of Ba in  $B_2O_3$  glass is higher than that of Ti, more Ba will be dissolved out from the  $BaTi_4O_9$ 



Fig. 3. (a) Bulk density of the  $BaTi_4O_9$  samples as functions of temperature and the content of  $B_2O_3$  and  $BaB_2O_4$ ; (b) porosity of the samples sintered at 1050 °C for 2 h as a function of the content of  $B_2O_3$  and  $BaB_2O_4$ .



Fig. 4. Microstructures of  $BaTi_4O_9$  samples sintered at 1050 °C for 2 h with addition of: (a) 9 wt%  $B_2O_3$ ; and (b) 9 wt%  $BaB_2O_4$ .

which will eventually results in the formation of  $TiO_2$  and  $Barich B_2O_3$  glasses.<sup>5,6</sup> At the same time, another reaction between  $BaTi_4O_9$  grains and Ba-rich  $B_2O_3$  glass will be proceeded, that which leads to the formation of the  $BaTi(BO_3)_2$  and  $Ba_2Ti_9O_{20}$  phases. On the other hand, when  $BaB_2O_4$  is added, less Ba will be dissolved out from  $BaTi_4O_9$  comparing to the case of  $B_2O_3$  addition because  $BaB_2O_4$  can be considered as a material that Ba component already dissolved in  $B_2O_3$ . In this case, no  $TiO_2$  will be produced but  $BaTi(BO_3)_2$  and  $Ba_2Ti_9O_{20}$  will be produced.

Fig. 3(a) shows bulk density of samples as functions of sintering temperature and the content of  $B_2O_3$  and  $BaB_2O_4$ . The bulk density increased as the sintering temperature increased. The overall tendency showed that the density of the samples with  $BaB_2O_4$  addition was higher than that of  $B_2O_3$  addition. Comparing the porosity of the samples sintered at 1050 °C for 2 h as a function of borides content, porosity increased with the content of  $B_2O_3$  in contrast to  $BaB_2O_4$  addition. In addition to the pores, phase development also influenced on the density of the samples. Since more  $B_2O_3$  addition leads to more production of  $BaTi(BO_3)_2$  ( $\rho = 4.2$  g/cm<sup>3</sup>) and TiO<sub>2</sub> ( $\rho = 4.2$  g/cm<sup>3</sup>) phases, which have lower density than  $Ba_2Ti_9O_{20}$  ( $\rho = 4.6$ g/cm<sup>3</sup>) phase, the decrease in bulk density is occurred as shown in Fig. 3(a).

Microstructures of sintered samples with 9 wt% of  $B_2O_3$  and  $BaB_2O_4$  are presented in Fig. 4. When 9 wt% of  $B_2O_3$  is added, large pores were observed. On the basis of energy dispersive



Fig. 5. Schematic diagram of intergranular pore development process: (a) before; and (b) after sintering when a liquid-forming additive of  $B_2O_3$  is added.

spectroscopy (EDS) and X-ray diffraction analysis, the phase of  $Ba_2Ti_9O_{20}$ ,  $BaTi(BO_3)_2$  and  $TiO_2$  were distinguishable in the microstructure. The shape of needle like and plate like grains of  $BaTi(BO_3)_2$  and  $Ba_2Ti_9O_{20}$  are well agreed with the previous observation.<sup>5,7</sup>

Fig. 5 shows the schematic diagram of intergranular pore development process which corresponds to the case of the sample with 9 wt% of  $B_2O_3$  as its microstructure is presented in Fig. 4(a). In a green pellet shown in Fig. 5(a), B<sub>2</sub>O<sub>3</sub> and BaTi<sub>4</sub>O<sub>9</sub> particles are homogeneously distributed. During sintering over the eutectic temperature of  $B_2O_3$ , the melts of  $B_2O_3$  will soak into the solid skeleton of BaTi<sub>4</sub>O<sub>9</sub> grains leaving behind voids at the place where the  $B_2O_3$  existed. Because of the reaction between B2O3 and BaTi4O9, most of the melts of B2O3 disappeared and the pore elimination through the liquid flow induced pore filling<sup>8</sup> is not available, which resulted in the generation of large pores observed in Fig. 4(a). From this point of view, it can be considered that the densification and reaction occur simultaneously during sintering process when both B<sub>2</sub>O<sub>3</sub> and BaB<sub>2</sub>O<sub>4</sub> are added. Since B2O3 addition induces complicated and much more chemical reactions than BaB<sub>2</sub>O<sub>4</sub> addition, densification might be delayed and densification starts at higher temperature



Fig. 6. (a) Dielectric constant; and (b) temperature coefficient of resonant frequency of samples sintered at 1050 °C for 2 h as a function of  $B_2O_3$  and  $BaB_2O_4$  content.

when  $B_2O_3$  is added as revealed in Fig. 3(a). Note that a great increase in densification occurred at 1000 and 1050 °C when  $BaB_2O_4$  and  $B_2O_3$  were added, respectively.

The dielectric constant of the samples sintered at 1050 °C for 2h as a function of B<sub>2</sub>O<sub>3</sub> and BaB<sub>2</sub>O<sub>4</sub> is presented in Fig. 6(a). For the B<sub>2</sub>O<sub>3</sub> added samples, dielectric constant slowly increased from 37.9 to 38.4 as the content increased from 1 to 5 wt%. Further addition of B<sub>2</sub>O<sub>3</sub> over 5 wt% resulted in a great decrease in dielectric constant. The increase in dielectric constant is thought to be originated from the formation of  $TiO_2$ phase, which has high dielectric constant around 105. The great decrease in dielectric constant over 5 wt% of B<sub>2</sub>O<sub>3</sub> is believed to be caused by poor densification since B<sub>2</sub>O<sub>3</sub> produces many large pores. As the content of  $BaB_2O_4$  is increased from 1 to 9 wt%, dielectric constant revealed almost constant value around 37.5 but showed an increasing tendency with BaB<sub>2</sub>O<sub>4</sub> content. Even though the formation of the  $BaTi(BO_3)_2$  was expected to reduce the dielectric constant due to its low dielectric constant around 11.5, the dielectric constant was not decreased. The negative effect of BaTi(BO<sub>3</sub>)<sub>2</sub> phase on dielectric constant seems compensated by the accelerated densification effect of BaB<sub>2</sub>O<sub>4</sub>. The quality factor  $(Q \times f)$  of the samples decreased with increasing

the content of B<sub>2</sub>O<sub>3</sub> and BaB<sub>2</sub>O<sub>4</sub>. When the content of B<sub>2</sub>O<sub>3</sub> is increased from 1 to 9 wt%, even though the figure is not presented, the quality factor decreased from 36,350 to 24,140, while the quality factor decreased from 38,860 to 33,370 as the content of BaB<sub>2</sub>O<sub>4</sub> increased from 1 to 9 wt%. Fig. 6(b) shows the temperature coefficient of resonant frequency ( $\tau_f$ ) of the samples sintered at 1050 °C for 2 h as a function of borides content.  $\tau_f$  increased with increasing of B<sub>2</sub>O<sub>3</sub> content. Since B<sub>2</sub>O<sub>3</sub> addition led to the formation of TiO<sub>2</sub>, it is thought that the TiO<sub>2</sub> second phase is attributed to the increase in  $\tau_f$  because TiO<sub>2</sub> has high positive  $\tau_f$  value. When BaB<sub>2</sub>O<sub>4</sub> is added, the  $\tau_f$  is nearly independent of the amount of BaB<sub>2</sub>O<sub>4</sub>.

### 4. Conclusion

The effect of low temperature glasses of borides addition on microwave dielectric characteristics and sintering behavior of BaTi<sub>4</sub>O<sub>9</sub> ceramics was examined. When B<sub>2</sub>O<sub>3</sub> was added, active dissolution of Ba and Ti into B<sub>2</sub>O<sub>3</sub> liquid from BaTi<sub>4</sub>O<sub>9</sub> led to the formation of many second phases during sintering process. Moreover, B<sub>2</sub>O<sub>3</sub> produced many large pores in the microstructure. These results made the dielectric characteristics of BaTi<sub>4</sub>O<sub>9</sub> deteriorated. When BaB<sub>2</sub>O<sub>4</sub> was added, chemical reaction between the glass and BaTi<sub>4</sub>O<sub>9</sub> seems to be suppressed and densification was improved, which results in superior dielectric characteristics than the case of B<sub>2</sub>O<sub>3</sub> addition.

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